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PREDICTION OF SPECIFIC FUEL CONSUMPTION IN TURBOCHARGED DIESEL ENGINES UNDER PARTIAL LOAD PERFORMANCE

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Abstract. It is known that the performance of Diesel engine at partial load is different from the performance at full load, but engines manufacturers usually provide only the operation characteristics in the highest efficiency condition. In order to determine the Diesel engine performance at all operation condition an investigation has been conducted. The purpose is to develop a theoretical model based on the iso-consumption curve of the IVECO 8360.46.417 Diesel engine that allows predicting the refuse trucks engine consumption used in this work. With the curve and the information provided by the manufacturer the prediction of the specific consumption and performance of a refuse truck turbocharged engine fueled by Diesel was made using a two-variables regression with a third grade polynomial approximation. The result is a third grade polynomial that allows the specific consumption calculation depending on the torque and the engine speed.

Key words

Diesel Engine, Simulation, Specific fuel consumption, Turbocharged, Iso-consumption curve.

1. Introduction

So far, mostly researches have been focused on Diesel engine operation in highest efficiency conditions. Mostly, Diesel engine manufacturers only provide the operation conditions in the highest steady-state performance, at full load. However, most of the daily driving cycles include operation at partial loads. Consequently, the investigation of Diesel engine operations at partial loads has become important in order to know its behavior at real operating parameters. It is important to determine significant deviations from the highest steady-state performance in the most important operation parameters that are: specific consumption, efficiency and emissions. The purpose of the present work is a theoretical model development that allows Diesel engine operation conditions based on the IVECO 8360.46.417 iso-consumption curve and the data provided by the engine manufacturer.

2. Problem Statement

In the design and manufacturing process of an engine many tests are carried out in order to know the performance under partial and full load. However, Diesel engines manufacturers provide datasheets with few information about the engines performance. In some cases, they only specify the consumption in the operation condition with highest efficiency, which is under full load. In other cases, the manufacturers provide the specific consumption in three operation conditions which are Peak Torque, Government Speed and Maximum Power. Nevertheless, it is important to know the specific consumption and the performance under partial load for any engine. For this reason, the main purpose of this work is the development of a theoretical polynomial that allows the engine specific fuel calculation in function of the torque and the engine speed.

3. Literature Review

The performance of Diesel engines under partial loads has been widely studied, since the specific consumption at partial loads becomes higher than at full loads [1] [2]. The same occurs even when there is natural gas - Diesel dual operation [3].

Many efforts to predict the engines specific fuel consumption have been carried out. The fuel consumption for tractor engines at a particular load is obtained from *ASAE D497, clause 3*, which establishes a related equation. A most general equation for annual consumption is given by *ASAE EP496.2 FEB03* [4]. These equations from ASAE have been tested (*R. Grisso*) and it was concluded that they predict accurately the fuel consumption under partial loads [5].

There are also efforts to establish mathematical models in order to predict the specific fuel consumption as a function of the Diesel engine working parameters and, thus, to model the engine iso-consumption curves, which are generally similar shaped for Diesel engines [2]. S. Popescu, I. Dumitru, S. Boruz and Z. Kiernicki propose a second-degree polynomial to determine a Diesel engine specific fuel consumption dependant on an effective engine torque and engine speed as well as to elaborate the optimum working curve, which represents the function of engine torque dependant on speed engine for which specific engine consumption is minimum for each power level [6].

Radan Durković and Milanko Damjanović present a regression model [7] in the form of a third-degree polynomial in the function of working parameters, effective pressure and number of revolutions, that predicts accurately the specific fuel consumption for Diesel engines.

4. Methodology

In the present work an outline of the procedure is given based on a regression model that has been presented in detail in previous publications [7]. As stated above, the main purpose of this work is the development of a theoretical polynomial that allows the specific fuel calculation in function of the torque and the engine speed. It is known that Diesel engines with similar characteristics have similar partial load performance [2]. For this reason, a specific fuel consumption curve corresponding to an engine whit similar characteristic to the refuse trucks ones was taken as a reference. To the development of the model, the IVECO 8360.46.417 iso-consumption curve was used (*Agudelo John, Doctoral Thesis* [8]) and it is shown below.

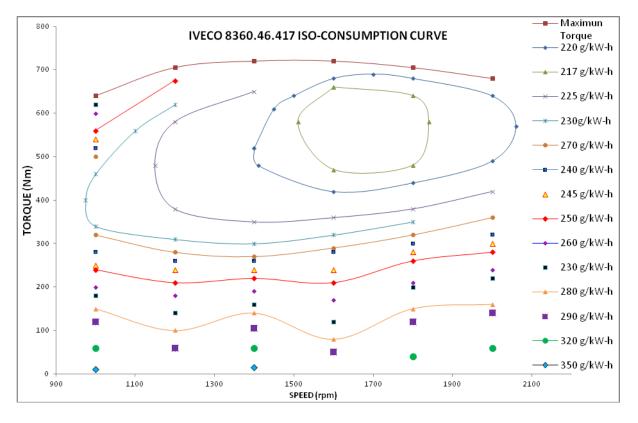


Fig. 1 – IVECO 8360.46.417 ISO-CONSUMPTION CURVE. Agudelo John, Doctoral Thesis [8]

The iso-consumption curve showed in *Figure 1* can be made dimensionless in order to re scaled it. Knowing the operation conditions of the studied engine at three operation points given by the manufacturer its specific fuel consumption curve can be predicted. To this end, the dimensionless curve has to be scaled in order to force the three given operation points to fit the curve. Once the iso-consumption curve is predicted, the specific fuel consumption is related to the efficiency coefficient, this is why it is so important to know its behavior. The relationship among them is as follows:

$$b_{e} = \frac{3600}{H_{u}.\eta_{M}} \left[\frac{kg}{kWh} \right] \tag{1}$$

Where; b_{ε} is the specific fuel consumption, $\eta_{\rm M}$ is the efficiency coefficient and $H_u \begin{bmatrix} k_f \\ k_g \end{bmatrix}$ is the fuel heating value. Generally, the specific fuel consumption is a nonlinear function of operation parameters, torque and engine speed, such as: $b_{\varepsilon} = f(X)$. Where,

$$X^{T} = [x_{1}, x_{2}, \dots, x_{n}]$$
 (2)

Is the vector of operation parameters. Now it is linearized in the vicinity of the working parameters at the working point by Taylor series:

$$\hat{b}_{e} \approx \sum_{j=0}^{k} \hat{a}_{j} \cdot f_{ij}(\mathbf{X}), \ i = 1, 2, ..., N$$
 (3)

By the application of the least square fit method:

$$R = \min \sum_{i=1}^{N} \left(b_{ei} - \hat{b}_{ei} \right) \text{ and } \frac{\partial R}{\partial \hat{a}_j} = 0, \quad (4)$$

Where j = 0, 1, ..., k.

Then, a system of ordinary equations is obtained:

$$\boldsymbol{F}^{T}.\,\boldsymbol{F}.\,\hat{\boldsymbol{a}} = \boldsymbol{F}^{T}.\,\hat{\boldsymbol{b}}_{\boldsymbol{e}} \tag{5}$$

Where f(X) defines the operation parameters at N of known values b_{ε} . And the vector of unknown coefficients of the regression equation is,

$$\hat{\boldsymbol{a}} = [\hat{a}_1 \ \hat{a}_2 \ \dots \ \hat{a}_k]^T \tag{6}$$

Then, the equations system is solved:

$$\widehat{a} = (F^T \cdot F)^{-1} \cdot F^T \cdot b_e \tag{7}$$

The recommendation is to use a third degree polynomial form for the regression [7]. So the next regression model was chosen:

$$\hat{b}_{e} = \hat{a}_{1} + \hat{a}_{2}T_{e} + \hat{a}_{3}n + \hat{a}_{4}T_{e}n + \hat{a}_{5}T_{e}^{2} + \hat{a}_{6}n^{2} + \hat{a}_{7}T_{e}n^{2} + \hat{a}_{9}T_{e}^{3} + \hat{a}_{9}n^{3} + \hat{a}_{10}T_{e}^{2}n$$

$$(8)$$

Where T_{ε} is the torque, in this case in HN.m, n is the speed in RPM, and \hat{b}_{ε} is the fuel consumption in g/kWh.

5. Results

As stated above, the data points are from a heavy duty turbocharged Diesel engine commonly used in refuse trucks. The engine datasheet provided by the manufacturer specifies the maximum rating performance data at three operation points which are Governed Speed, Maximum Power and Peak Torque. The information is shown in the table below.

	Governed Speed	Maximum Power	Peak Torque
Engine Speed	2200 RPM	2000 RPM	1300 RPM
Output Power	213 kW	224 kW	159 kW
Torque	922 N-m	1068 N-m	1166 N- m
Fuel Consumption	49.9 kg/h	49.9 kg/h	35.2 Kg/h

Table 1 – Maximum rating performance data

With the data showed in *Table 1*, the dimensionless isoconsumption curve from the IVECO 8360.46.417 was re scaled. The predicted iso-consumption curve of the studied engine is shown below:

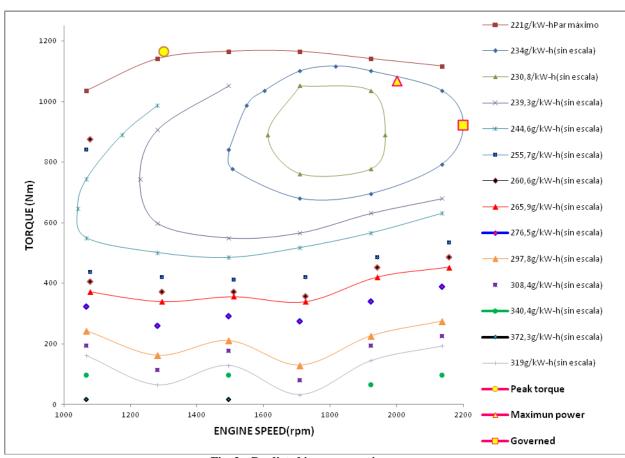


Fig. 2 – Predicted iso-consumption curve

In this study, 118 values of consumption and working parameters were used to obtain the coefficients.

The regression coefficients are obtained and the resulting polynomial is as follows:

(9)

 $\hat{b}_e = 420,814546410482 - 51,5882970028774T_e - 0,0215840453514n + 0,0241860678868T_en + 3,2893682520578{T_e}^2 - 0,000064862217n^2 - 0,0000083575876{T_e}n^2 - 0,1107606818463{T_e}^3 + 0,0000000308545n^3 + 0,0000494527209{T_e}^2n$

The specific fuel consumption curve is plotted and shown below:

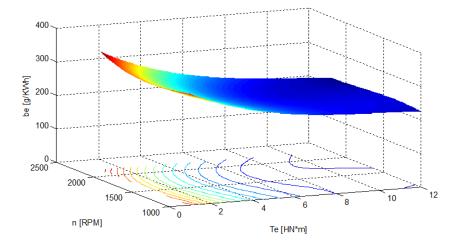
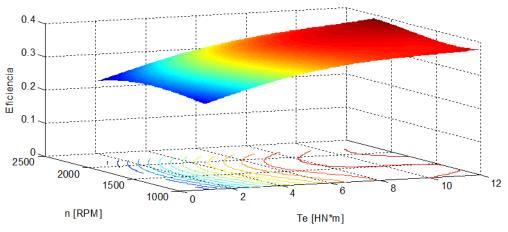


Fig. 3 – Predicted Specific fuel consumption curve

The efficiency curve can be also obtained:





LOAD PERCENTAGE	ERROR $\left[\frac{g}{kWh}\right]$
0-25	9,452667702
25-50	3,542929544
50-75	6,852723984
75-100	6,852723984

 Table 2 – Obtained error for different load percentage

 related to the maximum load

6. Conclusions

The proposed methodology allows predicting the specific consumption of a Diesel engine in any condition knowing little information about its performance, which, in some cases, is only about consumption in the operation condition with highest efficiency, under full load, or in other cases, in three operation conditions which are *Peak Torque, Government Speed* and *Maximum Power*

Knowing the specific consumption at any condition lets us also predict the overall consumption in urban traffic conditions, which would be useful in preventive maintenance and also in a pre-feasibility study of massive transport means.

7. Future Research

Furthermore, a proposed methodology to predict the efficiency behavior in dual operation at different fuel substitution percentages with natural gas is presented. It is important to get information about the performance in some operation points and at different substitution percentages; this would be drawn as follows:

Table	3 –	Future	research	parameters
Labie	•	1	i eseur en	parameters

	n_i	(rpm)	Scale Factor
Torque (N. m)	Efficiency	Substitution percentage x(%)	SF
	η _{i1}	0	1
T _{ej}	η_{i2}	x _{i2}	SF ₁
	η _{is}	x _{i3}	SF ₂
	η_{ik}	x _{ik}	SFk

A scale factor which shows the deviation of the efficiency at a particular substitution percentage from the base line efficiency is proposed. The base line is the efficiency for pure Diesel operation (x = 0%), the result obtained in the present work. A regression may be made in order to obtain the scale factor *SF* as a function of torque, engine speed and substitution percentage:

$$SF = SF(T_e, n, x) \tag{10}$$

Larger the number of known operation points, better the approximation obtained by the regression. Finally, the

efficiency can be scaled for each operation point and the efficiency can be shown as a function of torque, speed and substitution percentage:

$$\eta = \eta(T_{\varepsilon}, n, x). \tag{11}$$

8. Recommendations

Experimental tests must be carried out in order to get real information about the Diesel engine operation points. For future researches experimental data is also needed for modeling Diesel-natural gas dual operation behavior. Besides, it is important to classify Diesel engines according to their constructive characteristics before applying models.

9. References

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