

Electromagnetic Interference from a Wireless Power Transfer System: Experimental Results

Elena N. Baikova^{1,4}, Stanimir S. Valtchev¹, R. Melício^{2,3}, Vítor M. Pires³

¹FCT, Universidade NOVA, Lisbon, Portugal

²IDMEC/LAETA, Instituto Superior Técnico, Universidade de Lisboa, Lisbon, Portugal

³Departamento de Física, Escola de Ciências e Tecnologia, Universidade de Évora, Portugal

⁴Escola Superior de Tecnologia, Instituto Politécnico de Setúbal, Portugal

e-mail: ruimelicio@gmail.com

Abstract. The paper presents experimental results of measurement and analysis of the electromagnetic fields generated by wireless power transfer system and their possible interaction on data transmission channel. The energy transfer efficiency depends strongly both on the operation of the power transmitter and the operation of the receiver as well. Currently, in the Faculty of Science and Technology of the University Nova high power wireless power transfer systems are being constructed. For the coordination and optimization of the transmitter and receiver of the power transfer system, a set of microcontrollers is in development. The microcontrollers' mutual communication is of extreme importance especially when high intensity fields will induce highly undesired influence. The two (or more) controllers take the responsibility of the control in the transmitting and the receiving sides, correspondingly. The controllers are supposed to communicate with each other through a RF data channel. The WPT system with the induced electromagnetic interference voltages and currents may influence or completely disrupt the communication which will be a severe problem.

Key words

Experimental results, wireless power transfer, communication technology, electromagnetic interference.

1. Introduction

Wireless power transfer (WPT) is a promising technology which attracts attention of researchers and manufacturers [1]. In the area of low power the applications are already wide spread: laptops, mobile phones, PDA, wireless headphones, implants, razors, toothbrushes etc. In the same time the high power equipment is also eager to get rid of the wires too, e.g. the industry of intelligent machining systems, robots, the forklift trucks, and of course, electric and hybrid cars. Recently the great deal of attention has been focused on the wireless charging systems for electric vehicles (EV) [1].

Among the existent WPT technologies, the magnetic resonant coupling which was developed by Kurs *et al.* [2], is proven to be the most suitable to achieve efficient

energy transfer for the EV's wireless charging [1]-[4]. Magnetic resonance is based on the transfer of electrical energy between two coils that are tuned to resonate at the same frequency. This technology uses generally frequency above 100 kHz.

An important step is to combine the power transfer with bidirectional data transmission. However, such WPT system with the induced electromagnetic interference voltages and currents may influence or completely disrupt the communication which will be a severe problem. The simultaneous power and data exchange needs a proper choice of the modulation strategy and some ideas are proposed in the inductive powering systems [5],[6] and in the resonant systems [7]-[9].

The wireless power and data transmission system with resonant coils tuned at one single working frequency is analyzed in [5]-[7]. The transmitted working frequency is modulated at the same time by the data transmission. In order not to be influenced by the energy transfer the data transmission can be treated by different technical methods, as amplitude shift keying (ASK), frequency shift keying (FSK) and phase shift keying (PSK) modulation [5]-[7].

The feasibility of the power and the data receiver implementation with the application of amplitude modulation with a single antenna is proposed in [5]. The system of wireless power and data transmission described in [7] operates at a frequency of 13.56 MHz and allows simultaneous transmission of energy and data with speeds up to 1 Mb/s. The operation principle is the modulation of the carrier frequency by the information signal.

The contactless power and data transmission system that uses two pairs of resonant coils is shown in [8],[9]. The adopted solution is based not only on separated coils for power and information transmission, but also on specially shaped multiple frames. The special geometry of data coils reduces the mutual coupling between the power and data coils. This way the voltage induced by electromagnetic field of WPT system can be reduced the

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However, the described systems also have disadvantages. The data transmission rate and the transferred energy are limited. Furthermore, the construction of the resonant coil should ensure a sufficient isolation between the power and the data transmission systems, which is difficult to accomplish.

To minimize the interferences of magnetic fields, the

power transfer and the data transmission have to be separated from each other [10],[11]. In this case a data exchange is realized at much higher frequencies, particularly in the GHz order, keeping low frequency for the energy transfer.

Currently, in the Faculty of Science and Technology of the University Nova high power WPT systems are being constructed. The microcontrollers' mutual communication is of extreme importance especially when high intensity fields will induce highly undesired influence. The two (or more) controllers take the responsibility of the control in the transmitting and the receiving sides, correspondingly. The controllers are supposed to communicate with each other through a RF data channel.

This paper mainly focuses on EMC issues on wireless power transfer, including electromagnetic interference impact of WPT system on data wireless channel. As far as it is known, a wide overview of the EMC problems of wireless power transfer simultaneously with the wireless data transmission has not yet been reported [12]. Thus, this paper is the contribution in the field of EMC issues in the wireless power e data transmission systems. This paper is organized as follows. Section 2 presents the wireless data transmission (WDT) and the WPT modelling and the efficiency of the WPT system. Section 3 presents the experimental results. Finally, concluding remarks are given in Section 4.

2. WDT Simultaneously with WPT

In the systems generally described, the power and data transfer are transmitted through the near electromagnetic field which operates across relatively short distances, i.e., up to a few meters. Unfortunately, the near field operation limits the communication speed and energy transfer efficiency. To overcome these limitations a more efficient power and data transfer system is proposed to implement. In this system a bidirectional communication between the transmitter and receiver is created. For the coordination and optimization of the transmitter and receiver of the WPT system, a set of microcontrollers is in development. It is assumed that this system will transmit not only high density energy but also high-density (high speed) data through RF data channels. The simultaneous wireless powering and data communication transmitter and receiver block diagram studied in the Faculty of Science and Technology (FCT), University

Nova is shown in Figure 1.

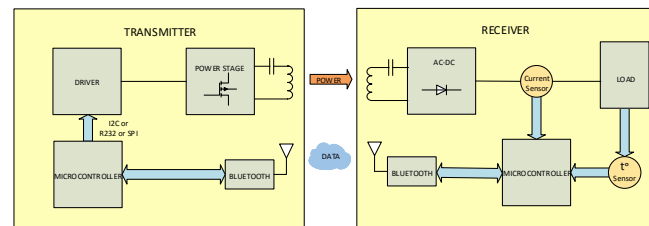


Fig. 1. Block diagram of wireless power transfer system.

The transmitter consists of a driver, a power stage, a transmitting coil and a microcontroller. The receiver side includes a receiving coil, an AC-DC rectification, a microcontroller and a current and temperature sensors respectively. The load is the EV battery. For the coordination between the transmitter and receiver and for operation optimization of the WPT system, a set of microcontrollers is in development.

A data transmission system with higher frequencies, i.e., on the order of GHz allows increasing the data transmission rate. In the case of exchange of information on advanced wireless transmission systems, several communication technologies could be adopted, such as Bluetooth, Wi-Fi, ZigBee [1],[11]. In this case the Bluetooth technology was adopted due to the fact that this standard is a compromise in terms of the data rate/efficiency/cost.

The schematic representation of a WPT system is shown in Figure 2. The schematic representation of a WPT system consisting on a two coils, where V_S is the AC power source, R_S is the resistance of the power source, R_1 , L_1 and C_1 are respectively the primary parasitic resistor, inductance and resonant capacitor, M_{12} is the mutual inductance between the primary and the secondary, R_2 , L_2 and C_2 are respectively the secondary parasitic resistor, inductance and resonant capacitor, R_L is the load resistance.

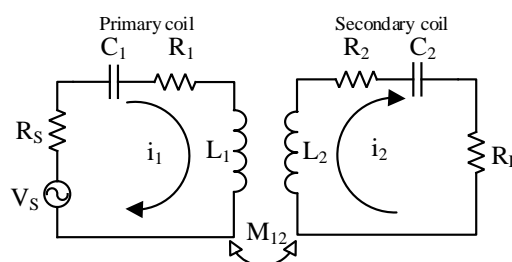


Fig. 2. Schematic representation of a WPT system.

The Kirchhoff's voltage law for the primary is given by

$$(R_s + R_1 + j\omega L_1 + \frac{1}{j\omega C_1})i_1 - j\omega M_{12} i_2 = v_s \quad (1)$$

The Kirchhoff's voltage law for the secondary is given by

$$(R_L + R_2 + j\omega L_2 + \frac{1}{j\omega C_2})i_2 - j\omega M_{12} i_1 = 0 \quad (2)$$

The loop impedances for the two coils is given by

$$Z_{12} = R_{SL} + R_{12} + j\omega L_{12} + \frac{1}{j\omega C_{12}} \quad (3)$$

The currents of primary and secondary are given by

$$I_1 = \frac{Z_2 v_S}{Z_1 Z_2 + \omega^2 M_{12}^2} \quad (4)$$

$$I_2 = \frac{j\omega M_{12} v_S}{Z_1 Z_2 + \omega^2 M_{12}^2} \quad (5)$$

At the resonance condition the reactive part of the impedance of the coils becomes zero. Therefore, at the resonant frequency the currents I_1 and I_2 can be simplified given by

$$I_1 = \frac{R_2' V_S}{R_1' R_2' + \omega^2 M_{12}^2} \quad (6)$$

$$I_2 = \frac{j\omega M_{12} V_S}{R_1' R_2' + \omega^2 M_{12}^2} \quad (7)$$

where R_1' and R_2' respectively are the total transmitting and receiving circuit resistances, is given by

$$R_1' = R_S + R_1 \quad (8)$$

$$R_2' = R_2 + R_L \quad (9)$$

The power of the input side P_{in} and output power delivered to the load P_{out} is given by

$$P_{in} = V_S I_1 \cos \varphi \quad (10)$$

$$P_{out} = I_2^2 R_L = \frac{R_L \omega^2 M_{12}^2 V_S^2}{(R_1' R_2' + \omega^2 M_{12}^2)^2} \quad (11)$$

The power transfer efficiency is given by

$$\eta = \frac{P_{out}}{P_{in}} = \frac{R_L \omega^2 M_{12}^2}{R_2' (R_1' R_2' + \omega^2 M_{12}^2) \cos \varphi} \quad (12)$$

In (12) the power transfer efficiency η is a function of the frequency and circuit parameters.

The efficiency decreases quickly when drift away from its resonant operation. High quality factor Q can increase the efficiency of the WPT system operating at resonance frequency.

3. Experimental Results

Electromagnetic interference (EMI) is important especially for the digital and analogue systems operating at 30 MHz to 300 MHz frequencies, where any circuit element becomes an antenna and can cause interference. The analysis was concentrated on the EM radiation caused by converter operating at 20 kHz switching frequency, at which the studied WPT system operates.

In principle, the EMI from a relatively low frequency, as expected in case, probably will be not so strong.

The Bluetooth technology operates at the frequency of 2.4 GHz which is enough higher than the first harmonic of the power transfer frequency (20 kHz). In order to verify this hypothesis some measurements and analysis were done.

The test equipment used to perform measurements was composed by an experimental setup of WPT system and the measurement system. The WPT system is shown in Figure 3 and consists of a high frequency power source, transmitting resonant coil, receiving resonant coil and electronic programmable load. The measurement equipment is shown in the Figure 4 consist of a basic unit, measuring instrument Narda SRM-3000 Selective Radiation Meter, a portable field strength meter, PMM 8053A, and antennas in 100 kHz ÷ 3 GHz frequency domain for the measurement of electromagnetic fields.

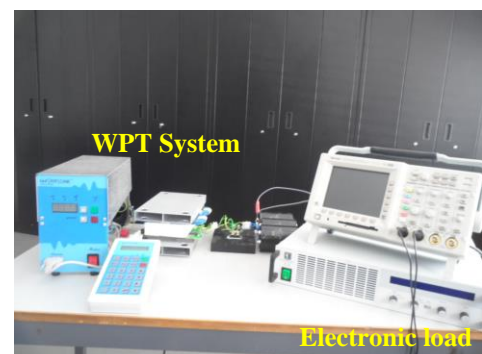


Fig. 3. WPT system: experimental setup.



Fig. 4. Measurement equipment.

The electric field intensity in WPT system for different power transferred levels taken in the Power Electronics Laboratory is shown in Figure 5. Figure 5 shows some disturbance at the frequency 1.9 MHz which may be

caused by the heavy consumption of nearby located smartphone. Because of this, in order to prevent external electromagnetic interference, the next series of measurements will be made inside a Faraday cage.

The results of electric field intensity in WPT system for different distances between the WPT equipment and the probe are shown in Figure 6.

The harmonic generation from WPT system operating at 20 kHz frequency is shown in Figure 7.

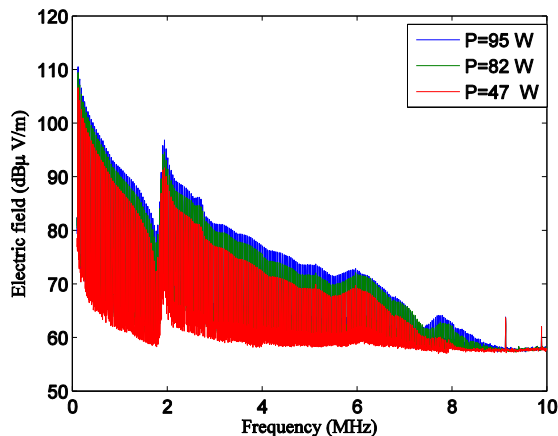


Fig. 5. Electric field intensity in WPT system for different levels of transferred power.

The used measurement equipment was capable to analyze frequencies starting from 100 kHz, so the amplitudes of the harmonics were measured starting from the 5th harmonic, corresponding to 100 kHz.

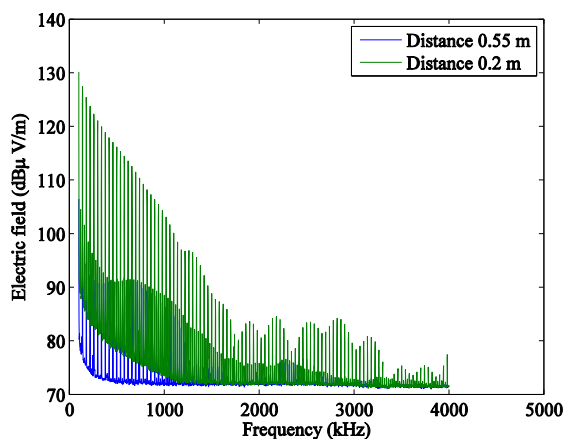


Fig. 6. Electric field intensity in WPT system for different distances.

To obtain the 1st harmonic and the 3rd harmonic amplitudes, the minimum squares method was used. Using the method of minimum squares the experimental data were adjusted with a coefficient of determination $R^2 = 0.9685$.

The high value obtained for R^2 value indicates that the trendline quite precisely fits the data. The amplitudes of the harmonics including the 1st harmonic and the 3rd one generated by WPT system is shown in Figure 8. The practical values of the

electric field E in function of distance from the WPT system is shown in Fig. 9.

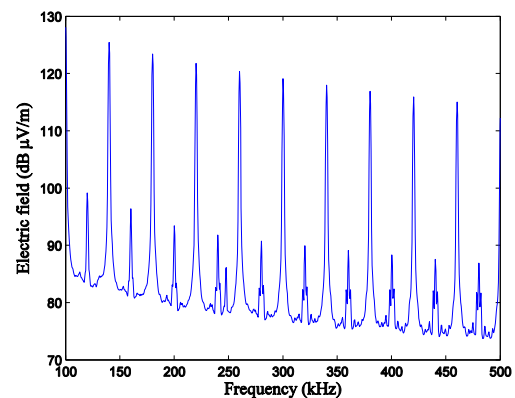


Fig. 7. Harmonic generation from the WPT system operating at 20 kHz frequency.

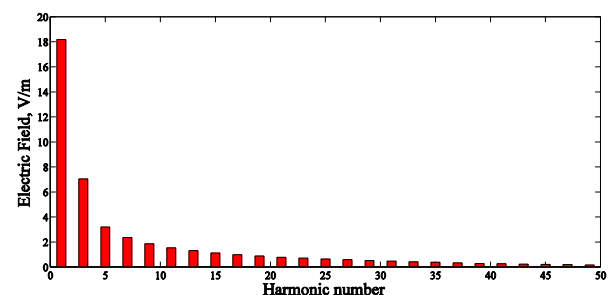


Fig. 8. Amplitude of the harmonics generated by the WPT system.

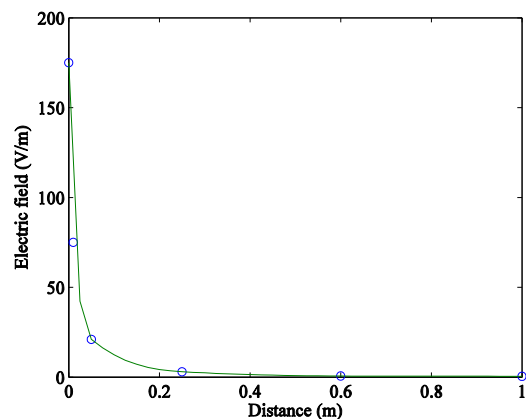


Fig. 9. Electric Field amplitude at the distance from the WPT system.

Figure 9 shows the electric field is much stronger directly adjacent to the WPT system but falls off rapidly with the distance.

The aim of these measurements is the evaluation of the electromagnetic fields levels generated by WPT systems. In order to estimate the electromagnetic interference impact on data wireless channel, it is necessary to evaluate the bit error rate (BER), the packet error rate (PER), or throughput of the communication system.

The most usual method to evaluate receiving quality of data wireless channel, including the effect of interference

